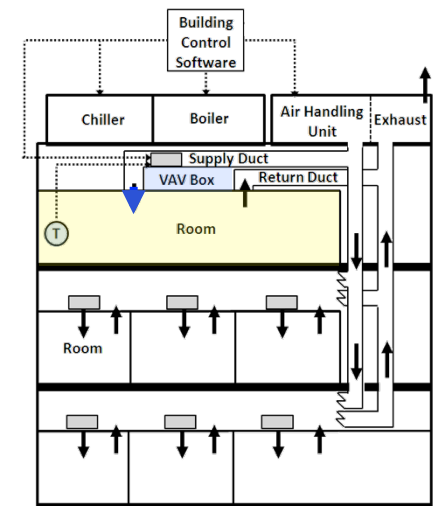
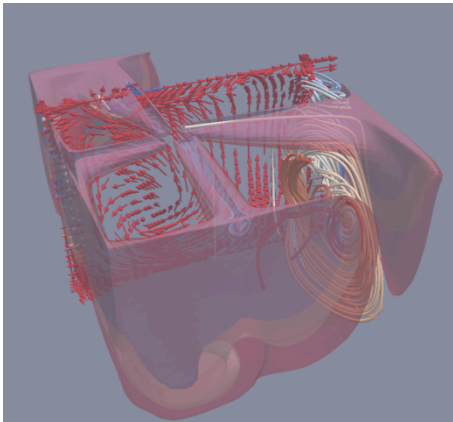


Software-Based Building Airflow Analysis Tool for Enabling HVAC Energy Use Savings in Commercial Buildings**

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** A work in progress



OUTLINE

- Introduction
- Motivation
- Solution
- Proof of Concept
- Commercialization

ACKNOWLEDGMENTS

CO-CONSPIRATOR



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Boston University

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- BU Facility Management



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PECI

FirstFuel

BuildingIQ

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Sebesta Blomberg

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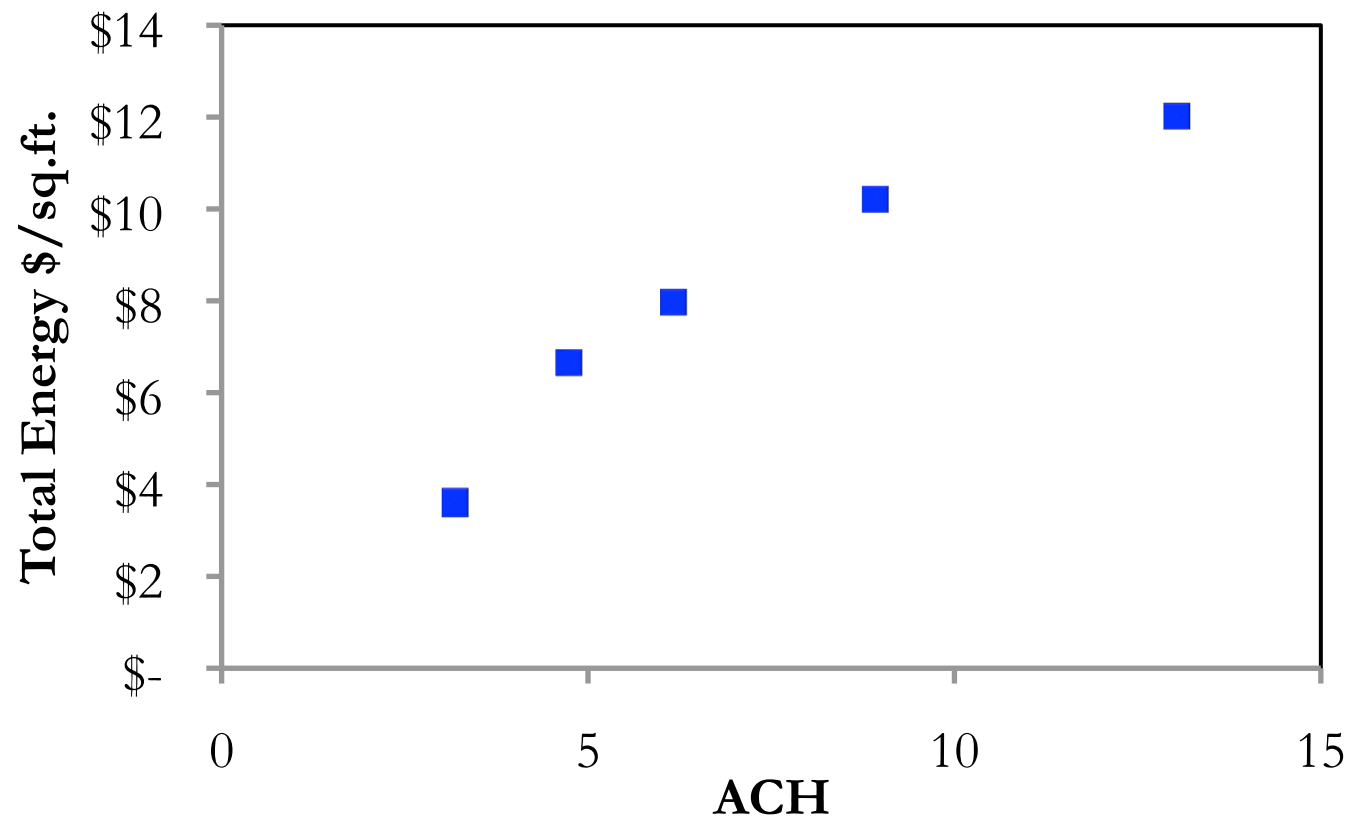
GreenerU

Rockport Capital

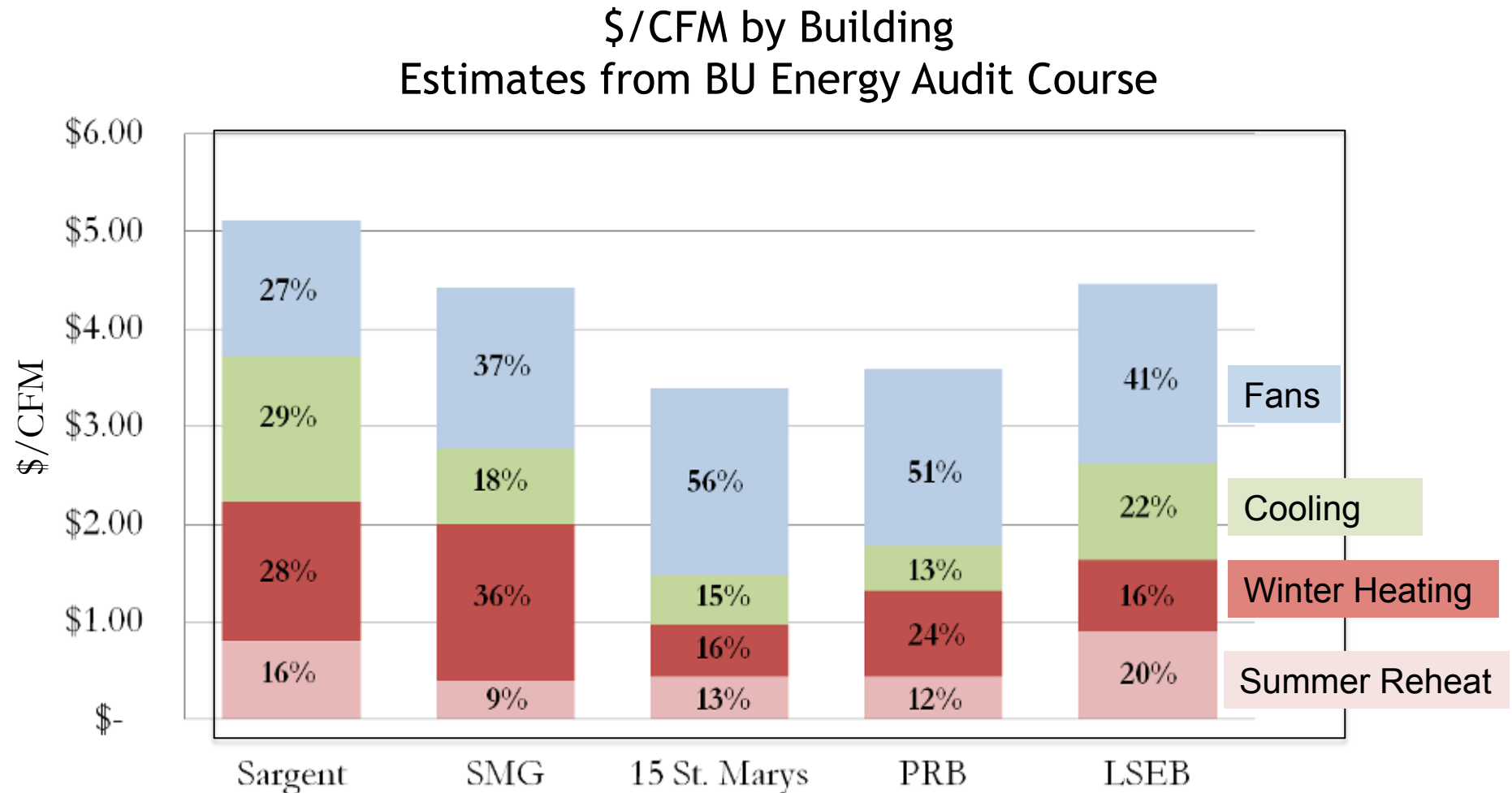
BU ENERGY AUDIT COURSE

Building Energy Costs Scale with Airflow rate

Overall Building Air Changes per Hour vs. \$/sq.ft.



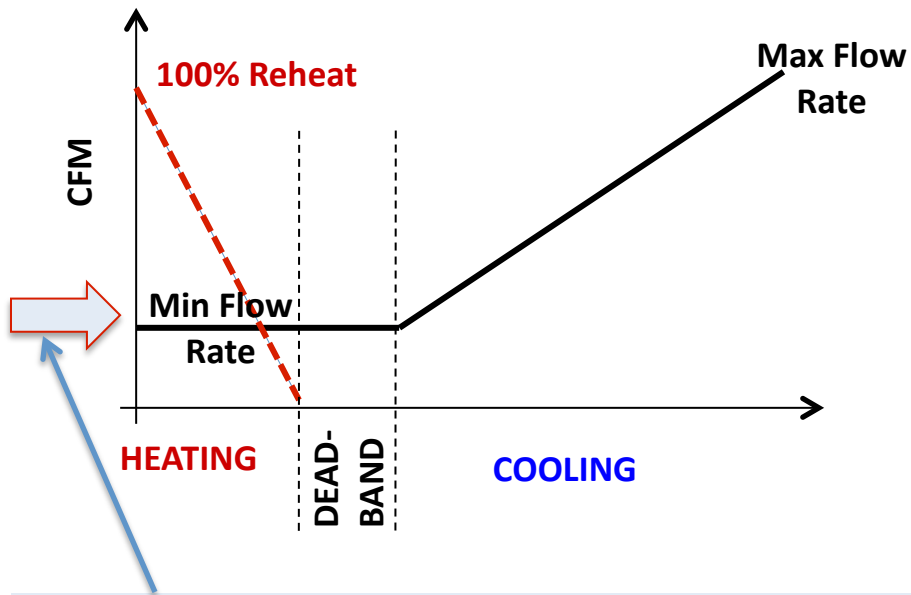
FAN ENERGY IS SIGNIFICANT PART OF \$/CFM



MOTIVATION

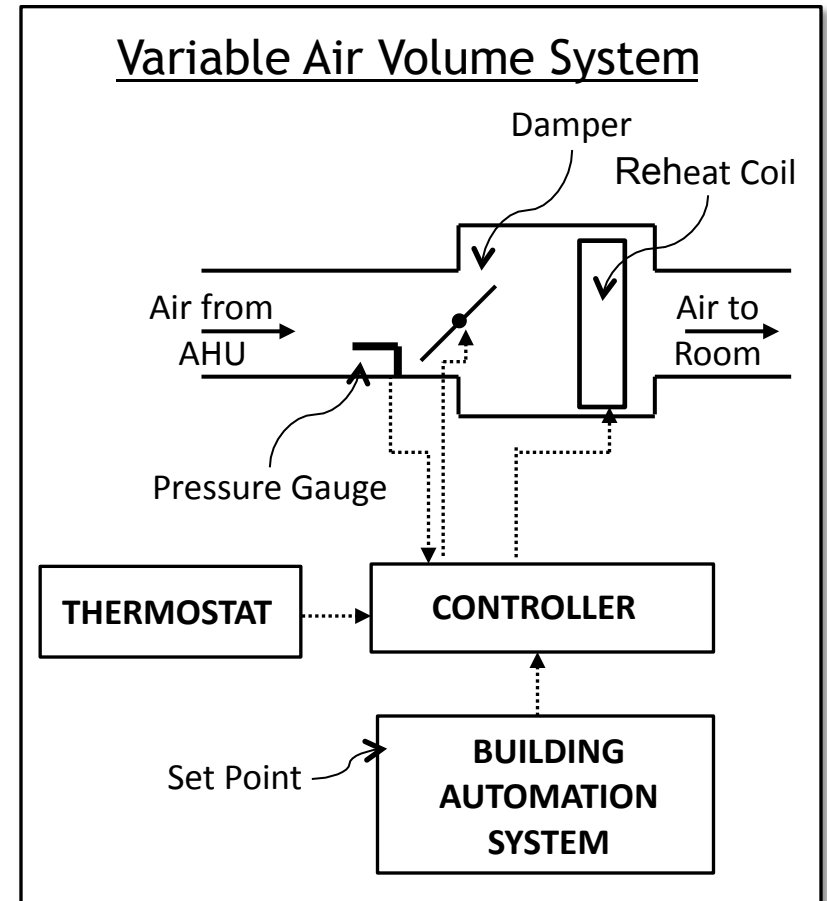
REDUCE MINIMUM VAV AIRFLOW SETTING

Single Max VAV Control Method



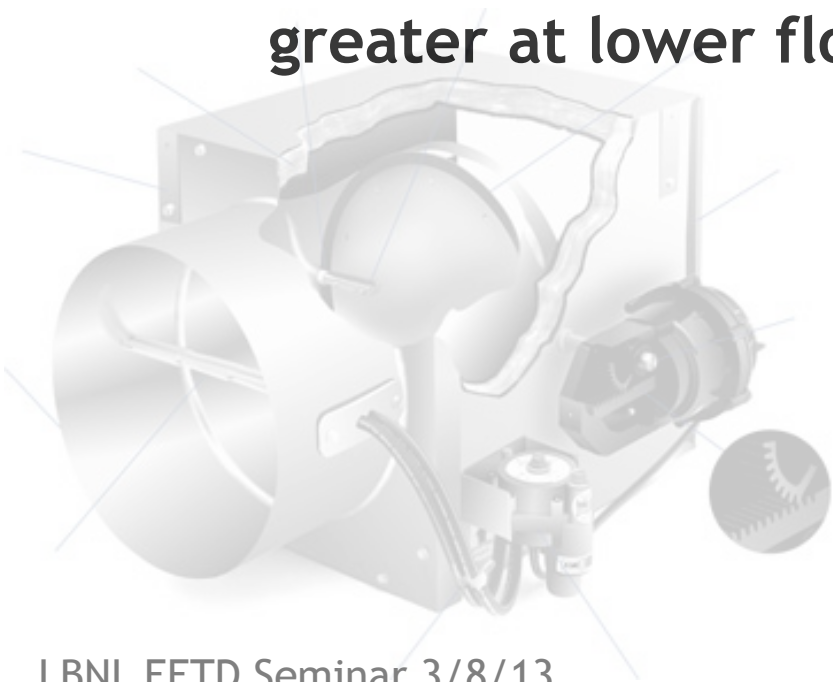
Minimum Air Flow typically set higher than code requirements*

Advanced VAV System Design Guide, 2003



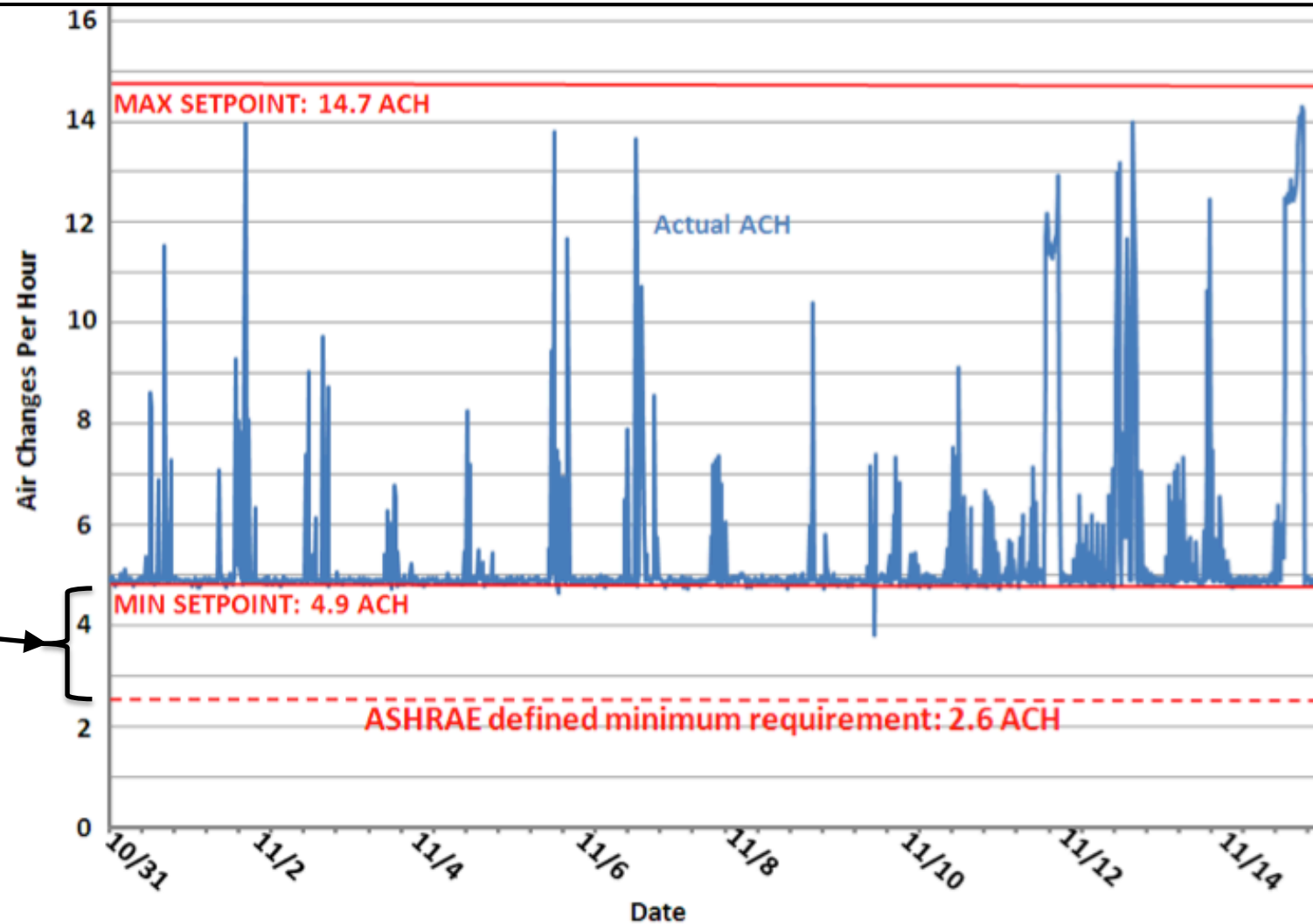
REDUCE MINIMUM VAV AIRFLOW SETTING

- **Blanc, 2007: VAV controllable down to 10% of design flow**
- **Arens, 2011: 24-30% HVAC energy savings by reducing minimum from 30 to 10% of max.**
- **Fisk, et al, 1997: Air Change Effectiveness is greater at lower flow rates**



MOTIVATION

POTENTIAL FOR SAVINGS



Minimum Air Flow set 38% Higher Ventilation Requirement

MOTIVATION

SETTING MINIMUM AIR FLOWS: NEW APPROACH NEEDED

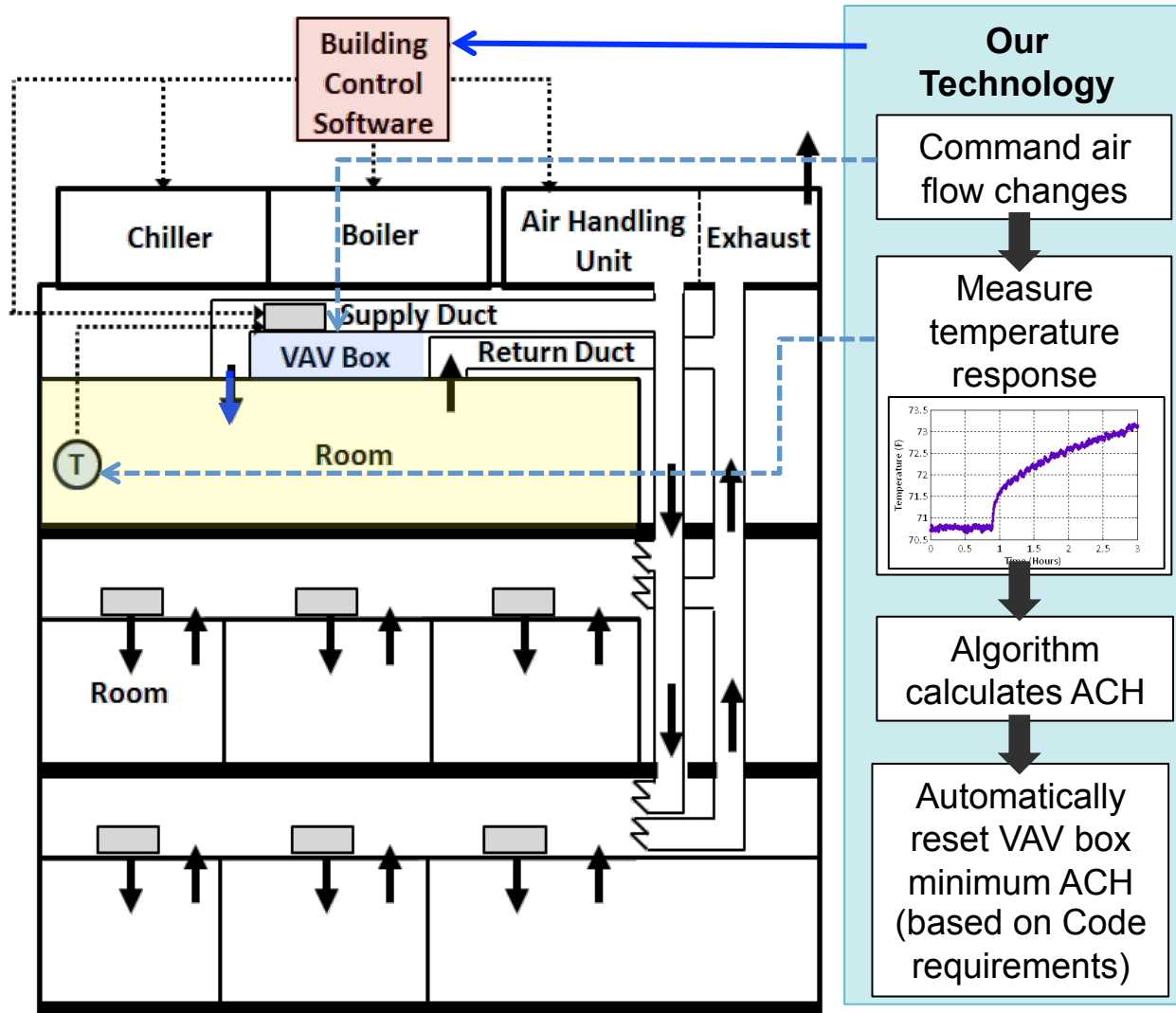
Manually Measuring Airflow



Labor Intensive
Time Consuming
Only first step in process
Ideally measure ACH

OBJECTIVE: Develop more cost effective way to measure ACH and reset minimums

OUR SYSTEM ID SOFTWARE APPROACH

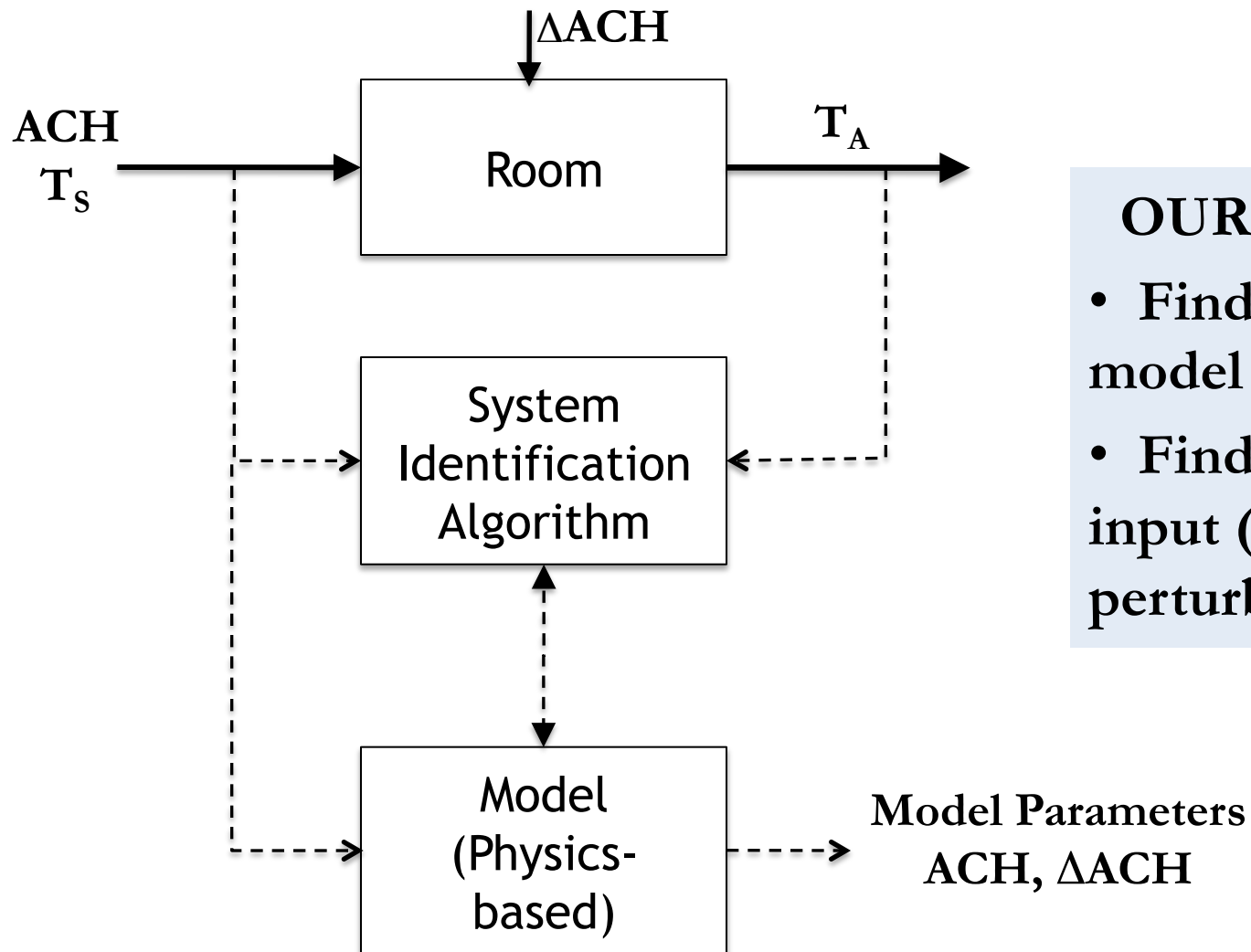


Software approach enables fully integrated solutions

Room-by-room results aggregable for building level savings

Enables monitoring & diagnostics

SYSTEM IDENTIFICATION

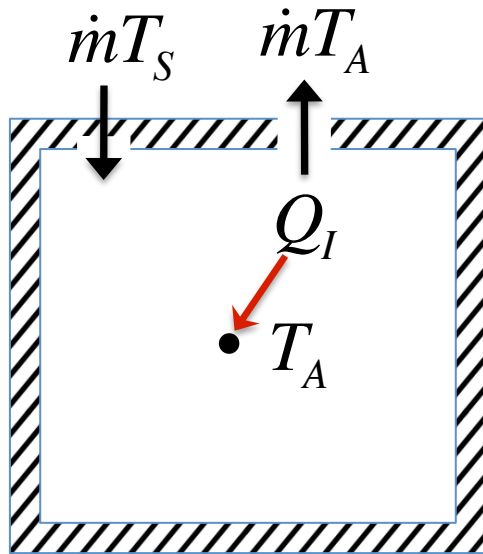


OUR APPROACH

- Find unknown model parameters
- Find unknown input (ACH) and perturbation (ΔACH)

1st ORDER SI MODEL

Fully Insulated Interior Room



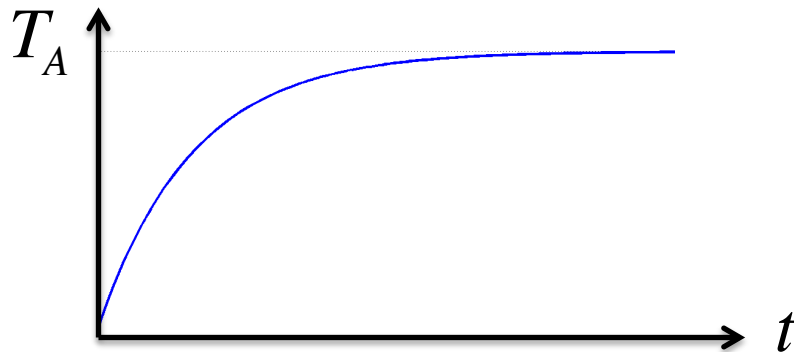
$$C_A \frac{dT_A}{dt} = \dot{m}c_p(T_S - T_A) + Q_I$$

$$T_A = T_{A,SS} + \alpha e^{\lambda t}$$

1st Order Response

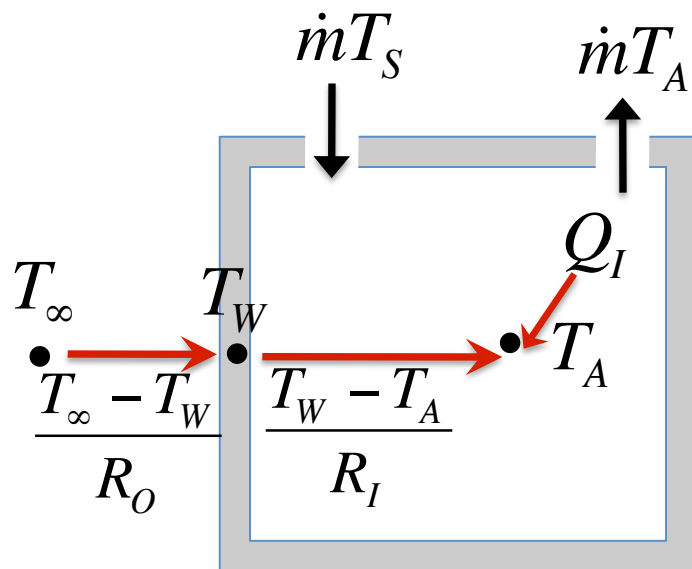
$$\tau = -\frac{1}{\lambda} = \frac{1}{ACH}$$

(Air Change Rate)



SECOND ORDER MODEL

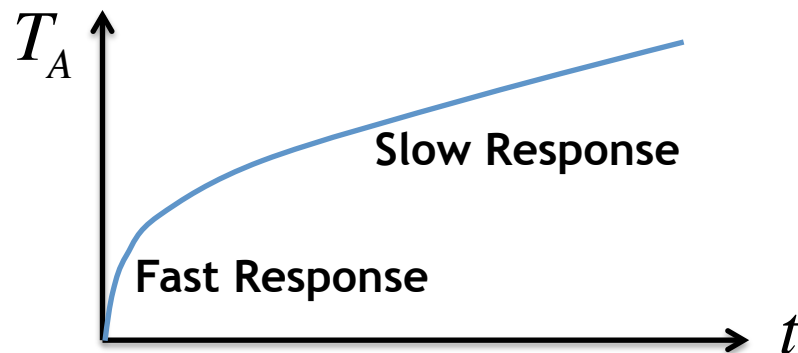
Heat transfer: air ↔ walls



$$C_A \frac{dT_A}{dt} = \dot{m}c_p(T_S - T_A) + Q_I + \frac{T_W - T_A}{R_I}$$

$$C_W \frac{dT_W}{dt} = \frac{T_\infty - T_W}{R_O} + \frac{T_A - T_W}{R_I}$$

$$T_A = T_{A,SS} + \alpha_1 e^{\lambda_1 t} + \alpha_2 e^{\lambda_2 t}$$



2nd Order Response with fast and slow time constants

$$\lambda_1, \lambda_2 = fn(ACH, C_A, C_W, R_O, R_I)$$

TRANSFER FUNCTION APPROACH: LAPLACE TRANSFORMS

Impose Step change in ACH

$$T_A = T_{A,SS} + \alpha_1 e^{\lambda_1 t} + \alpha_2 e^{\lambda_2 t}$$

$$\bar{T}_A(s) \equiv \int_0^{\infty} e^{-st} T_A(t) dt$$

Transfer
Function

$$\bar{T}_A(s) = \left[\frac{(T_s - \bar{T}_0) \left(s + \frac{1}{R_I C_W} + \frac{1}{R_O C_W} \right) \frac{1}{s}}{(s - \lambda_1)(s - \lambda_2)} \right] \Delta ACH$$

$$\lambda = -\frac{1}{2} \left(ACH + \frac{1}{R_I C_A} + \frac{1}{R_I C_W} + \frac{1}{R_O C_W} \right)$$

Poles=1/time constant

$$\pm \frac{1}{2} \sqrt{\left(ACH + \frac{1}{R_I C_A} + \frac{1}{R_I C_W} + \frac{1}{R_O C_W} \right)^2 - 4 \left(\frac{ACH}{R_I C_W} + \frac{ACH}{R_O C_W} + \frac{1}{R_I C_A R_O C_W} \right)}$$

FIRST ORDER ASYMPTOTIC SOLUTION

$$C_W \gg C_A$$

Fast Response

$$C_A \frac{dT_A}{dt} = \dot{m}c_p(T_S - T_A) + Q_I + \frac{T_W - T_A}{R_I}$$

$$\hat{\lambda}_1 = ACH + \frac{1}{R_I C_A}$$

Slow Response

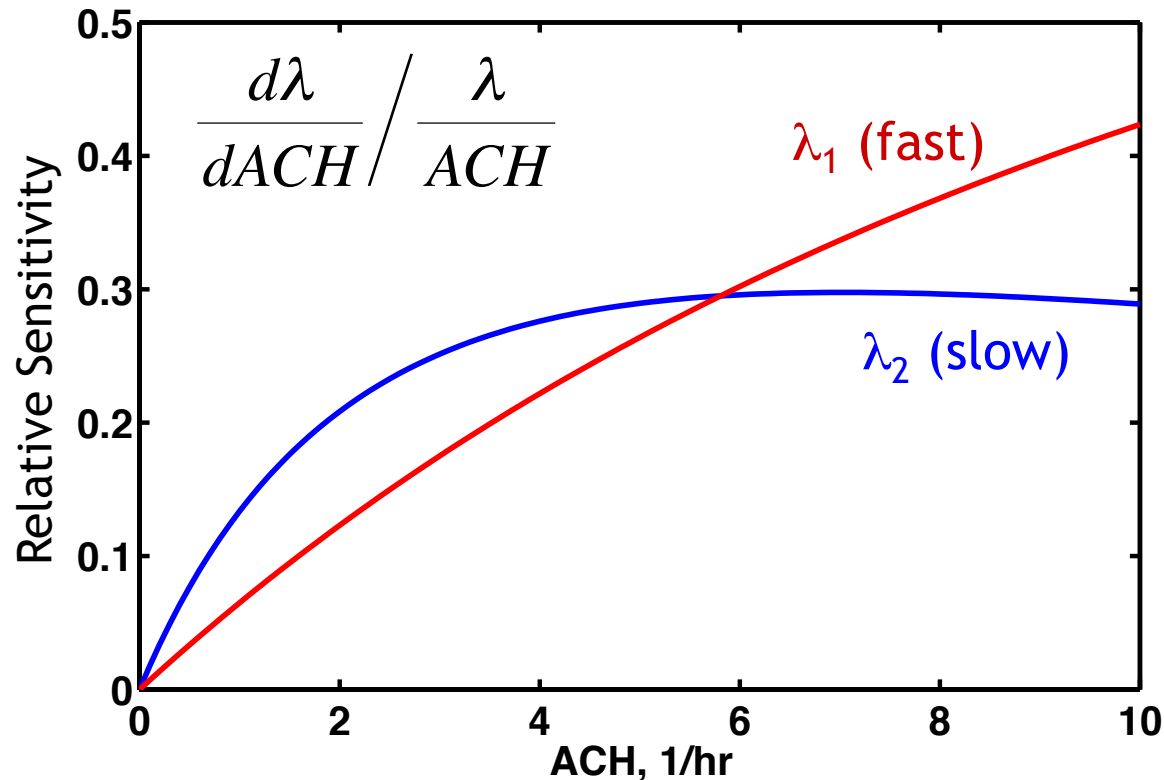
$$0 = \dot{m}c_p(T_S - T_A) + Q_I + \frac{T_W - T_A}{R_I}$$

$$C_W \frac{dT_W}{dt} = \frac{T_\infty - T_W}{R_O} + \frac{T_A - T_W}{R_I}$$

$$\hat{\lambda}_2 = \frac{1}{R_I C_W} \left[1 - \left\{ \left(ACH + \frac{1}{R_I C_A} \right) R_I C_A \right\}^{-1} \right] + \frac{1}{R_O C_W}$$

POLE SENSITIVITY TO ACH

Relative Sensitivity of λ_1 and λ_2



Relative sensitivity
of slow pole is
better than fast pole
for $ACH < 6$

$$\lambda = -\frac{1}{2} \left(ACH + \frac{1}{R_I C_A} + \frac{1}{R_I C_W} + \frac{1}{R_O C_W} \right) \pm \frac{1}{2} \sqrt{\left(ACH + \frac{1}{R_I C_A} + \frac{1}{R_I C_W} + \frac{1}{R_O C_W} \right)^2 - 4 \left(\frac{ACH}{R_I C_W} + \frac{ACH}{R_O C_W} + \frac{1}{R_I C_A R_O C_W} \right)}$$

SUMMARY OF SI APPROACH

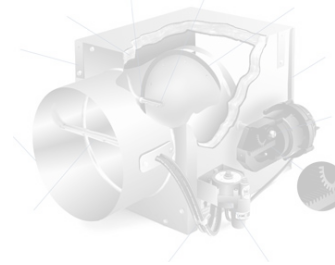
Change VAV box
flow rate (ACH)



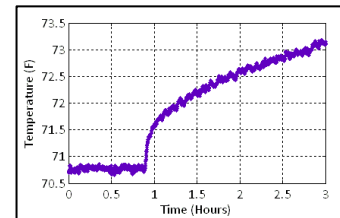
Fit second order
equation to
temperature response
(e.g., NLLS)



Extract ACH from
fit constants



$$T_A = T_{A,SS} + \alpha_1 e^{-\lambda_1 t} + \alpha_2 e^{-\lambda_{21} t}$$

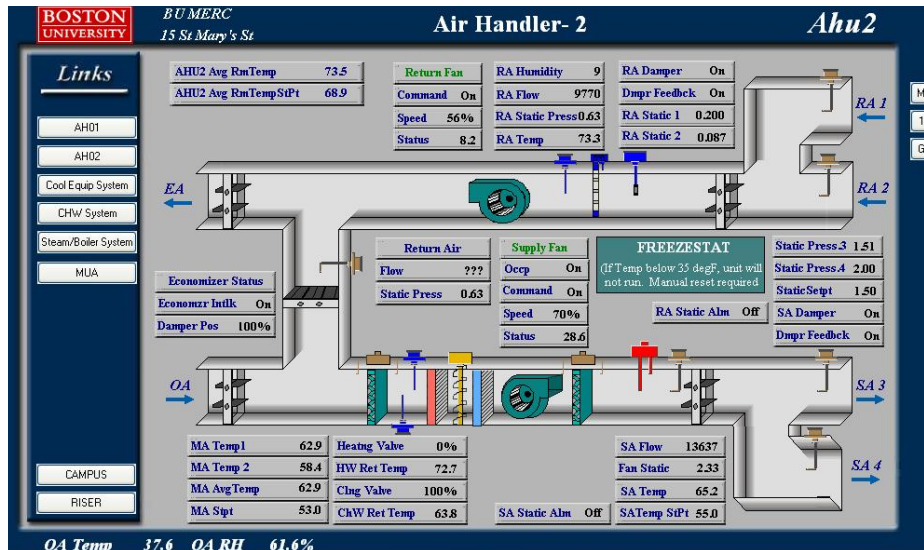


$$\lambda = -\frac{1}{2} \left(ACR + \frac{1}{R_I C_A} + \frac{1}{R_I C_W} + \frac{1}{R_O C_W} \right) \pm \frac{1}{2} \sqrt{\left(ACR + \frac{1}{R_I C_A} + \frac{1}{R_I C_W} + \frac{1}{R_O C_W} \right)^2 - 4 \left(\frac{ACR}{R_I C_W} + \frac{ACR}{R_O C_W} + \frac{1}{R_I C_A R_O C_W} \right)}$$

CHALLENGE:

Design experimental protocol to facilitate
ACH extraction with highest accuracy

EXPERIMENTS AT B.U.



Schneider Electric Continuum Workstation



TC-instrumented Room

- Occupied zone
- Dummy t'stat
- Wall
- Exhaust & Supply Vents
- Primary air zone

Balometer for initial and final flow rates

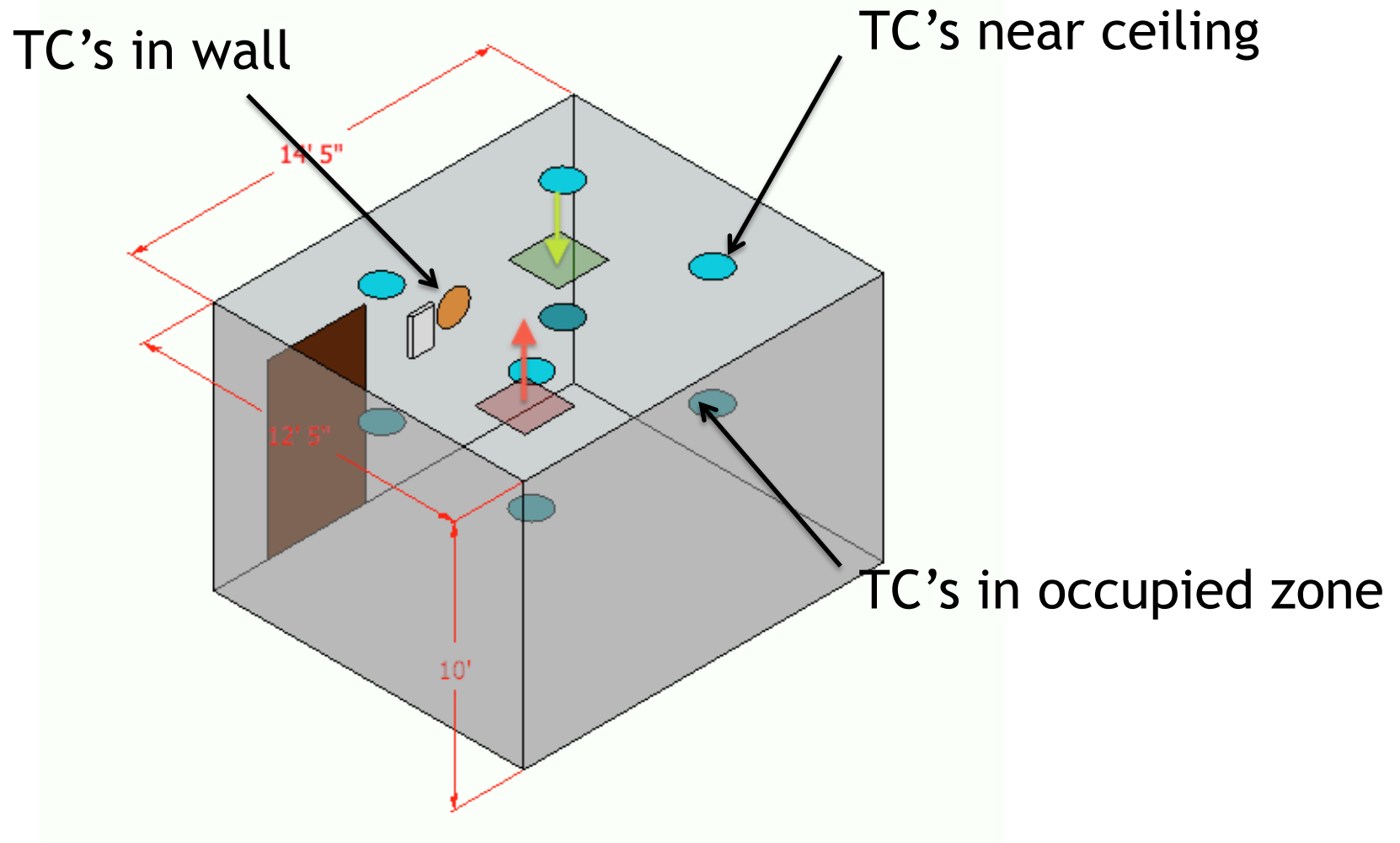


EXPERIMENTS AT B.U.

Building	Room Number	Room Type	Floor Area (ft ²)	No. VAV Boxes	No. Tests Run
15 St Mary's Street	136	Office	150	1	50
15 St Mary's Street	150	Classroom	698	2	10
15 St Mary's Street	124	Computer Lab	1261	2	5
15 St Mary's Street	131	Office	176	1	10
Photonics	B11C	Laboratory	618	3	5
Photonics	B14	Office	158	1	20
Photonics	736A	Lab Office	100	1	10

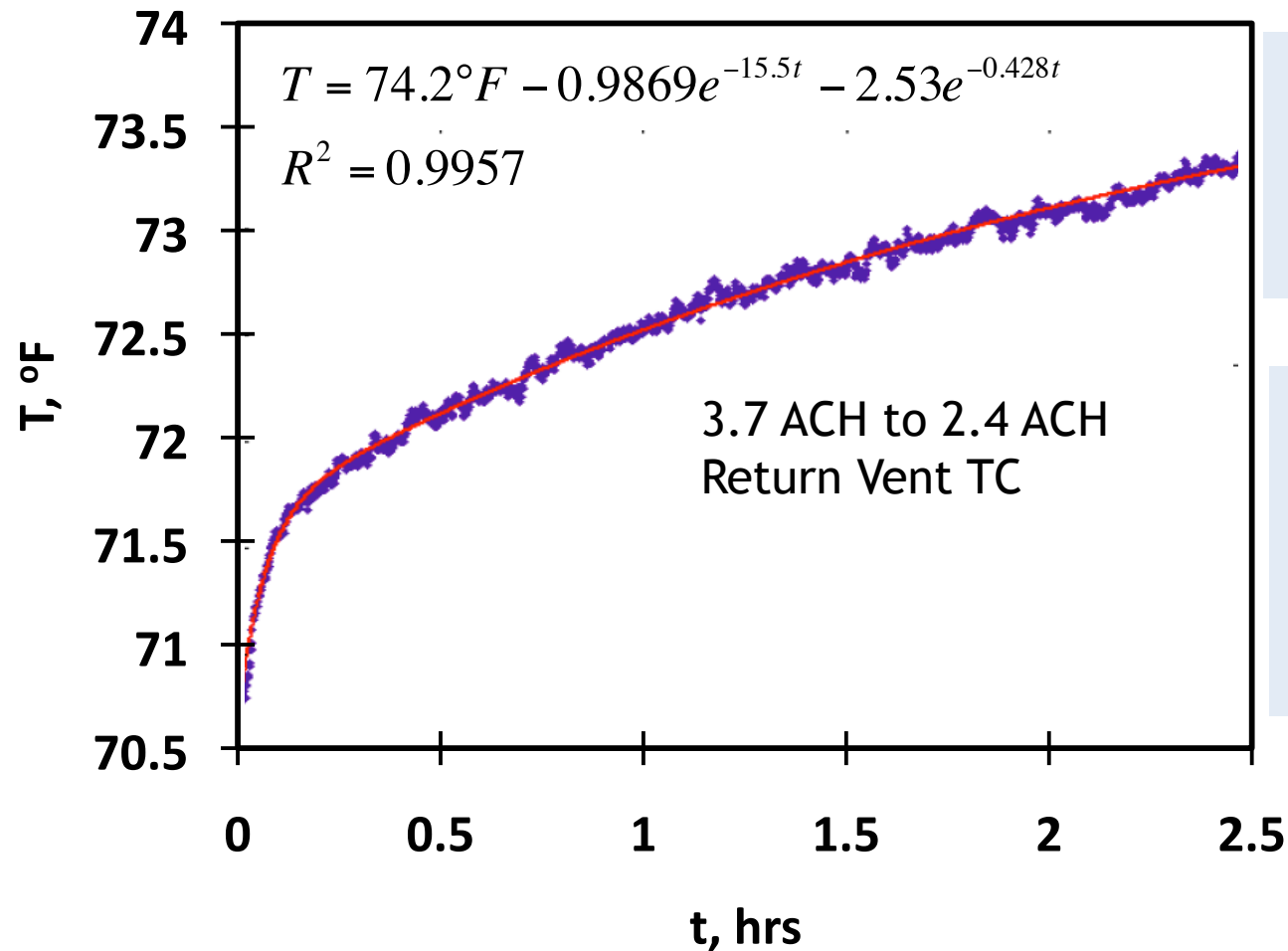


RM 136 15 ST MARYS



VERIFICATION OF 2ND ORDER RESPONSE: EXPERIMENT

Rm 136, 15 St Mary's Street
9/27/12



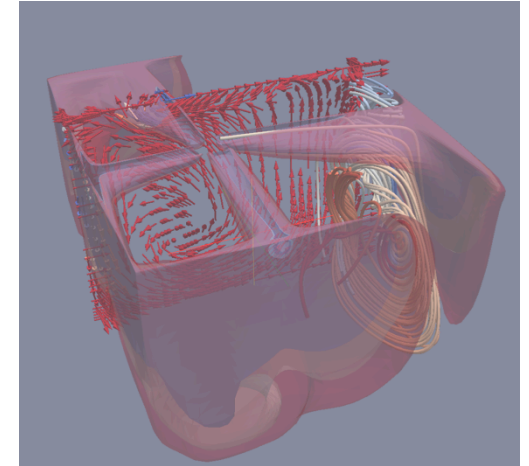
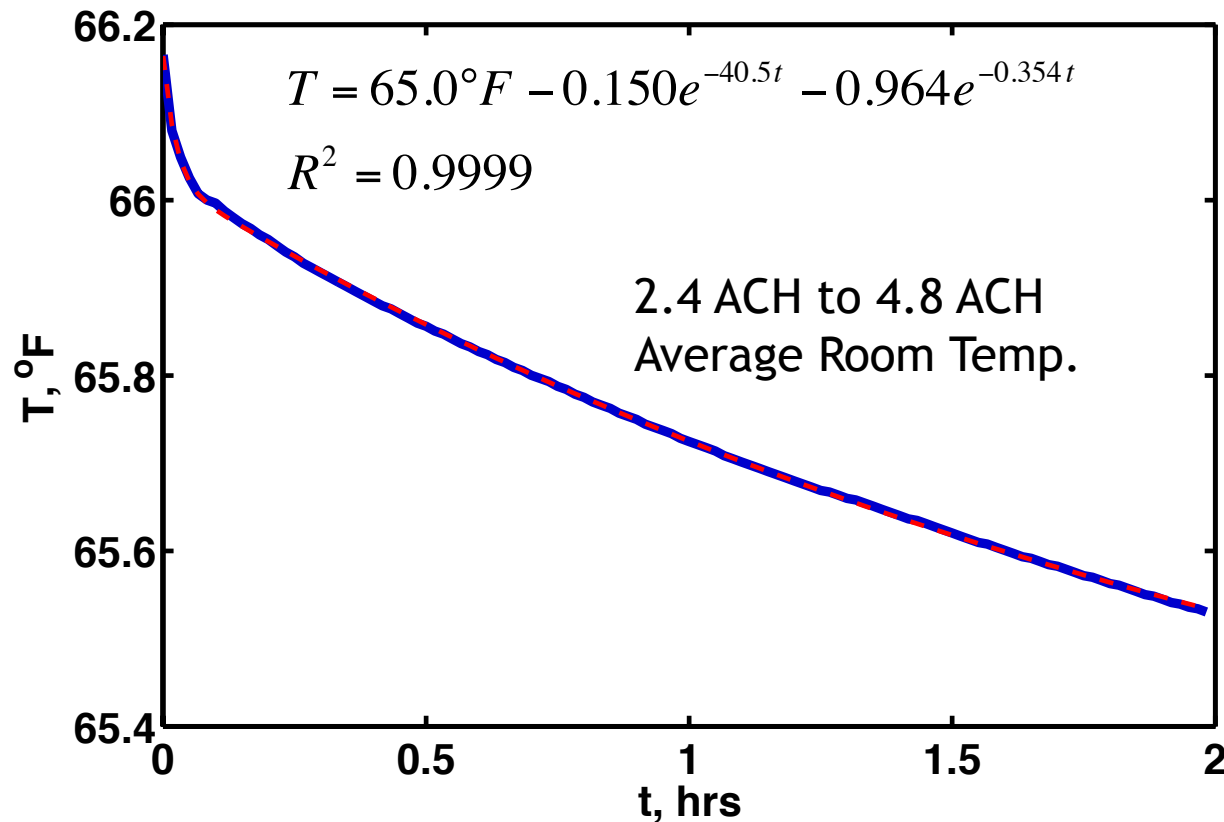
**2nd Order Response
Fits Experimental
Response**

**Model Captures
Key Physics:
Wall-Air Thermal
Coupling**

VERIFICATION OF 2ND ORDER RESPONSE: CFD

CFD using OpenFoam

Model of Rm 136, 15 St Mary's Street



**2nd Order
Response also
good fit for CFD**

UNKNOWN PARAMETER EXPERIMENTS

Determined fit constants
from test A

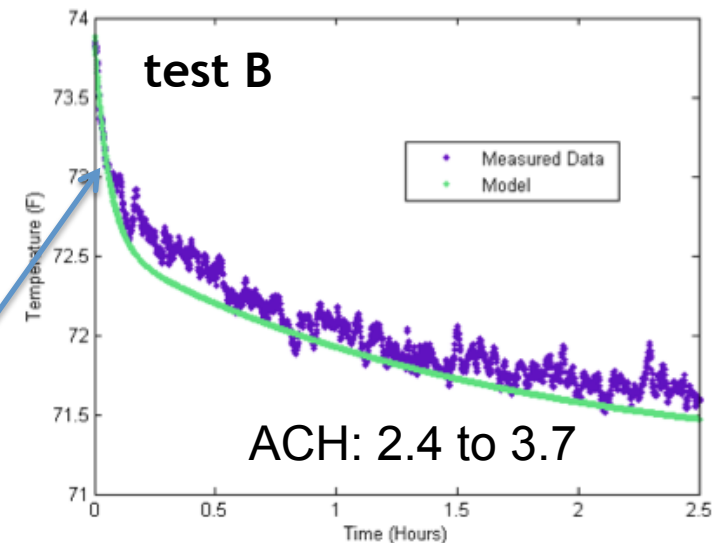
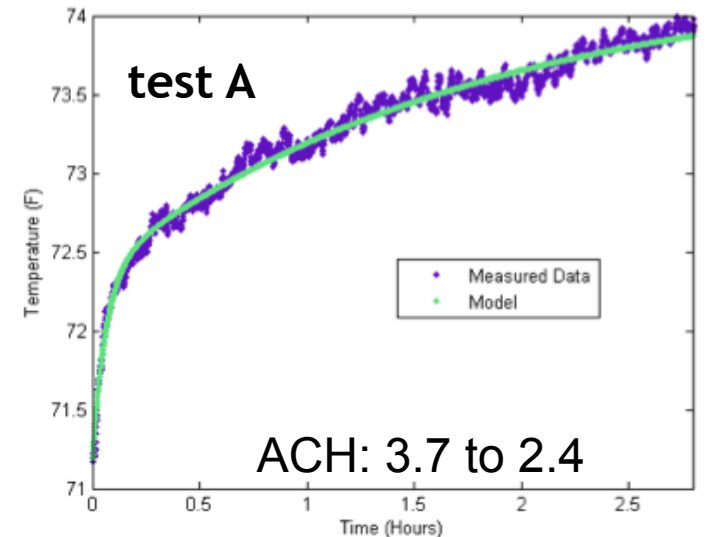


Used known parameters
 ACH , ΔACH , C_A , C_W , T_S
to estimate unknown
parameters
 R_I , R_O , Q_I , T_∞



Model w/ Full parameter set
compared with test B

Initial Fast Response Well Predicted



SI TECHNIQUE: PARAMETER GROUPING

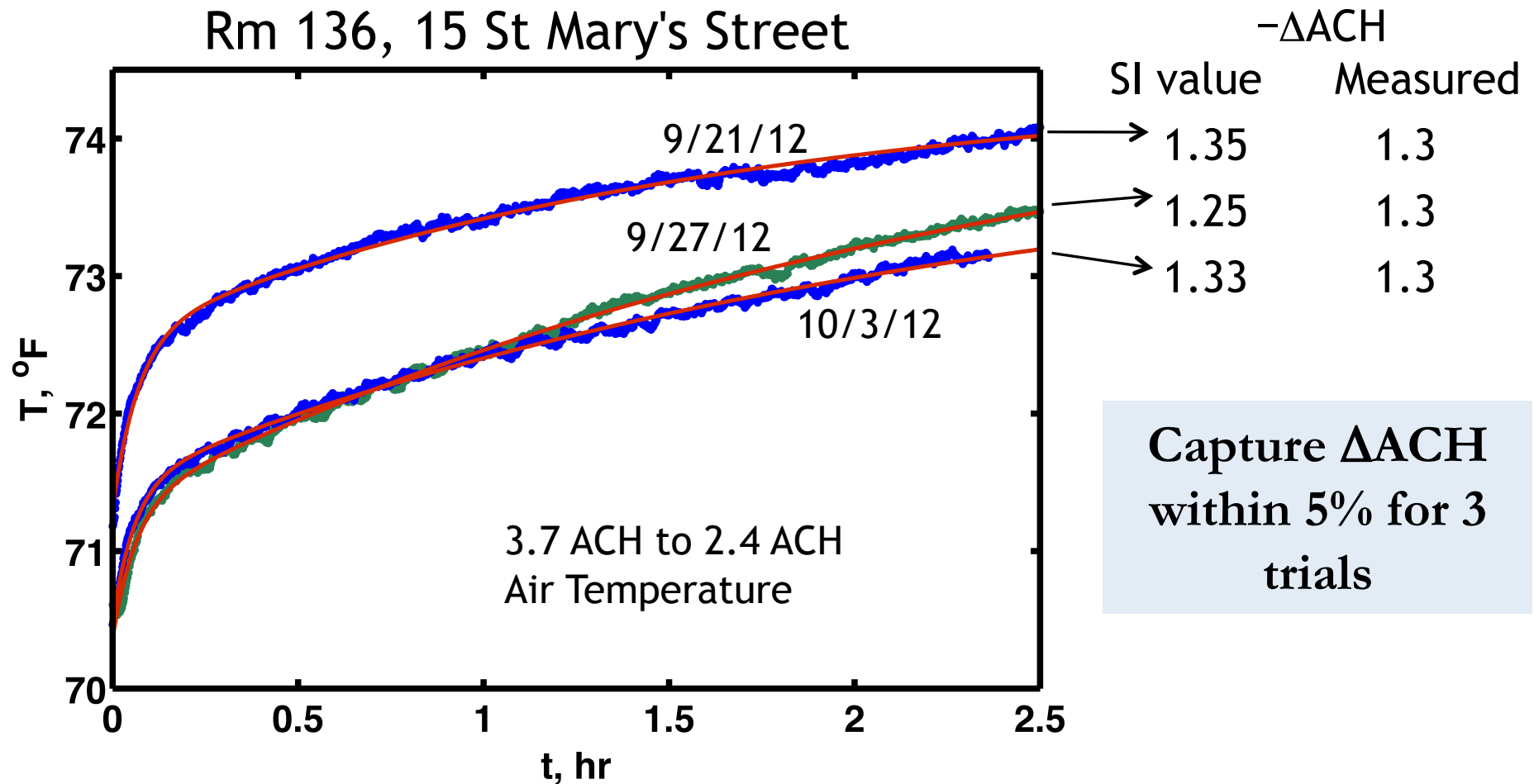
$$T_A = T_{A,SS} + \alpha_1 e^{\lambda_1 t} + \alpha_2 e^{\lambda_2 t}$$

$$\lambda_1, \lambda_2 = fn(a, b, c, d, T_{A,SS}, T_{A,0})$$

$$\alpha_1, \alpha_2 = fn(\lambda_1, \lambda_2, a, c, T_S, T_{A,0})$$

$$a = \frac{1}{R_I C_W} + \frac{1}{R_O C_W} \quad b = ACH \quad c = \Delta ACH \quad d = \frac{1}{R_I C_A}$$

ACH EXTRACTION: EXPERIMENT



COMMERCIALIZATION OPPORTUNITY

Building Market: >100,000 sq. ft. with BAS

Building Segment	Size (Million Sq ft)	Potential Savings (Million \$)**
M.U.S.H.*	6,222	622
Commercial	4,581	458

* Municipalities, Universities, Schools, Hospitals

** Based on average energy costs. Many cities have higher costs



- **Significant Market Opportunity**
- **Office buildings**
 - **Lower payback required**

COMMERCIALIZATION CHALLENGES

Aligning value offered with
decision authority

**Start with Owner-Occupied
Office Buildings**

Competitive and segmented
landscape

Differentiation

Low Cost, Software-Based

Low payback period

Full Solution

Upfront Analytics

Accessing Markets

Strategic Business Partnering

ESCO– MUSH market

New Untested Technology

Strategic Technical Partnering

_Building-Scale Demonstrations

COMMERCIALIZATION STATUS



Boston University School of Management
Institute for Technology Entrepreneurship & Commercialization

New Venture Competition Finalists

AUTOMATED TECHNIQUE OF MEASURING ROOM AIR CHANGE RATES IN HVAC SYSTEMS

U.S. Provisional Patent Application No.: 61/561,131

International Application No.: PCT/US2012/065786

SUMMARY

- Room thermal dynamics follows 2nd order response based on air-wall thermal coupling
- SI/software approach for measuring ACH
- Proof of concept experiments on BU buildings
- Future work
 - Refine SI extraction approach
 - Integration with BAS
 - Large-scale testing & implementation